

This Page Is Inserted by IFW Operations
and is not a part of the Official Record

BEST AVAILABLE IMAGES

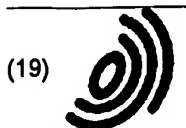
Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

IMAGES ARE BEST AVAILABLE COPY.

**As rescanning documents *will not* correct images,
please do not report the images to the
Image Problem Mailbox.**



(12)

EUROPEAN PATENT SPECIFICATION

(45) Date of publication and mention
of the grant of the patent:
28.02.2001 Bulletin 2001/09

(51) Int. Cl. : H04B 10/17

(21) Application number: 98306552.5

(22) Date of filing: 18.08.1998

(54) Optical fiber communication system with a distributed raman amplifier and a remotely pumped er-doped fiber amplifier

Faseroptisches Übertragungssystem mit einem verteilten Ramanverstärker und einem ferngepumpten Erbium-dotierten Faserverstärker

Système de communication à fibre optique avec un amplificateur Raman distribué et un amplificateur à fibre dopée-Erbium pompé à distance

(84) Designated Contracting States:
DE FR GB IT

(30) Priority: 28.08.1997 US 921984

(43) Date of publication of application:
24.03.1999 Bulletin 1999/12

(73) Proprietors:
, LUCENT TECHNOLOGIES INC.
Murray Hill, New Jersey 07974-0636 (US)
, Tyco Submarine Systems Ltd.
Morristown, NJ 07962 (US)

(72) Inventors:
, Kidorf, Howard David
Red Bank, New Jersey 07701 (US)
, Walker, Kenneth Lee
New Providence, New Jersey 07974 (US)

(74) Representative:
Watts, Christopher Malcolm Kelway, Dr. et al
Lucent Technologies (UK) Ltd,
5 Mornington Road
Woodford Green Essex IG8 OTU (GB)

(56) References cited:
EP-A- 0 476 830 EP-A- 0 789 432

(56) References cited:
, MASUDA H ET AL: "ULTRA-WIDEBAND
OPTICAL AMPLIFICATION WITH 3 DB
BANDWIDTH OF 65 NM USING A GAIN-
EQUALISED TWO-STAGE ERBIUM-DOPED
FIBRE AMPLIFIER AND RAMAN
AMPLIFICATION" ELECTRONICS LETTERS, vol.
33, no. 9, 24 April 1997, page 753/754
XP000695310
, AIDA K ET AL: "DESIGN AND PERFORMANCE
OF A LONG-SPAN IM/DD OPTICAL
TRANSMISSION SYSTEM USING REMOTELY
PUMPED OPTICAL AMPLIFIERS" IEE
PROCEEDINGS J. OPTOELECTRONICS, vol.
137, no. 4, 1 August 1990, pages 225-229,
XP000148979
, KAZUO AIDA ET AL: "LONG-SPAN
REPEATERLESS IM/DD OPTICAL
TRANSMISSION EXPERIMENT OVER 300KM
USING OPTICAL AMPLIFIERS"
COMMUNICATIONS - RISING TO THE HEIGHTS,
DENVER, JUNE 23 - 26, 1991, vol. 3, no. __, 23
June 1991, pages 1228-1232, XP000277531
INSTITUTE OF ELECTRICAL AND
ELECTRONICS ENGINEERS

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid. (Art. 99(1) European Patent Convention).

EP 0 903 876 B1

Description

Field of the Invention

[0001] This invention pertains to remotely pumped optical fiber communication systems that comprise optical fiber amplifiers.

Background

[0002] Optical fiber communication systems with remotely pumped Er-doped fiber amplifiers (EDFAs) are known. See, for instance, US patent 5,323,404, which shows a system with a single EDFA disposed between transmitter and receiver, with the pump source at the transmitter, and with the pump radiation being transmitted to the EDFA through the transmission fiber. See also P. B. Hansen, OFC '95, San Diego, California, February 1995, PD25.

[0003] Optical fiber communication systems with remotely pumped EDFAs are not limited to the single EDFA type disclosed in the '404 patent, but can have any number of EDFAs (or possibly other rare earth-doped fiber amplifiers). Herein a system will be considered a "remotely pumped" optical fiber communication system if the system comprises at least one discrete optical fiber amplifier (typically an EDFA), with the source of pump radiation for the discrete amplifier being spaced from the discrete amplifier, with the pump radiation being transmitted to the discrete amplifier through the transmission fiber such that the transmission fiber acts as a distributed Raman amplifier for the signal radiation. As is well known, in conventional silica-based single mode fiber the peak Raman gain occurs for pump radiation of wavelength λ_p about 100 nm less than the signal radiation wavelength λ_s , which typically is about 1.55 μm . This corresponds to a frequency shift of about 13 THz, as can be seen from FIG. 3 herein.

[0004] The use of high power pump sources in remotely pumped optical fiber communication systems can have advantageous results, including low noise amplification and high output power. Furthermore, such use can make possible increased distance between adjacent repeaters, typically resulting in lower system cost and higher reliability.

[0005] High power (e.g., > 1W) pump sources are known. See, for instance, S. G. Grubb et al., "Optical Amplifiers and Their Applications", Davos, Switzerland, p. 197, June 1995.

[0006] K. Aida et al., IEEE Proceedings Vol. 137, PtJ, No. 4, pages 225-229, disclose an optical transmission system with remotely pumped optical amplifier and Raman amplifier, with pump wavelength of 1.45 - 1.49 μm or 1.495 μm .

[0007] H. Masuto et al., Electronics Letters, Vol. 33, No. 9, pages 753-754, disclose wideband optical amplification by means of a 2-stage Er-doped amplifier and Raman amplification.

[0008] Despite the advantages provided by the use of high power pump sources in remotely pumped optical fiber communication systems, such use has drawbacks, especially in repeatered systems. For instance, we find that high pump power can result in multi-path interference (MPI) due to large Raman gain and Rayleigh scattering in the transmission medium. Thus, it would be desirable to have available a remotely pumped optical fiber communication system that substantially retains the advantageous characteristics of prior art systems with high pump power, but that is less subject to MPI. This application discloses such systems.

Summary of the Invention

[0009] The invention is defined by the claims. In a broad aspect the invention is embodied in a remotely pumped optical fiber communication system that is less subject to MPI than analogous prior art systems. Briefly, this is achieved by appropriate selection of the pump wavelength, namely, such that the pump wavelength is longer than the optimal wavelength for pumping the Raman amplifier, and longer than the optimal wavelength for pumping the EDFA, all for a given signal wavelength. The optimal wavelength for pumping the Raman amplifier herein is designated $\lambda_{p,Raman}$, and the optimal wavelength for pumping the EDFA herein is designated $\lambda_{p,EDFA}$. By the "optimal" wavelength of pumping an amplifier we mean that wavelength that gives the best combination of characteristics, typically including gain and noise figure.

[0010] For conventional signal wavelengths of about 1.55 μm , conventional silica-based transmission fiber and conventional EDFAs, $\lambda_{p,Raman}$ is typically about 1450 nm, and $\lambda_{p,EDFA}$ is typically about 1480 nm.

[0011] The design philosophy of remotely pumped fiber communication systems according to the invention involves selection of the pump such that the pump wavelength is not optimal for either the EDFA or the Raman amplifier, but yields improved over-all results through reduced MPI.

[0012] More specifically, the invention is embodied in an optical fiber communication system (typically a multi-wavelength system) that comprises a transmitter, a receiver, a transmission link that signal-transmissively connects the transmitter and the receiver and comprises at least one EDFA, and a source of pump radiation of

wavelength λ_p less than a signal radiation wavelength λ_s . The source of pump radiation is spaced from the EDFA, with the pump radiation being transmitted to the EDFA through at least a portion of the transmission link that comprises silica-based single mode optical fiber selected to provide Raman gain at λ_s . Significantly, λ_p is selected to be longer than $\lambda_{p,Raman}$, an optimal wavelength for producing said Raman gain, and also longer than $\lambda_{p,EDFA}$, an optimal wavelength for pumping the EDFA, with λ_p selected to result in reduced multi-path interference. For conventional signal wavelengths of about 1.55 μm , λ_p typically is in the approximate range 1490-1510 nm.

Brief Description of the Drawings

[0013]

FIG. 1 schematically depicts a multi-span remotely pumped optical fiber communication system;

FIG. 2 shows schematically one span of a communication system of the type shown in FIG. 1;

FIG. 3 shows Raman gain as a function of frequency shift;

FIG. 4 shows exemplary data on signal to noise ratio as a function of pump wavelength, for $\lambda_s = 1558$ nm;

FIG. 5 shows data on gain and noise figure as a function of wavelength, for an exemplary EDFA;

FIG. 6 schematically shows a portion of an exemplary multi-stage remotely pumped optical fiber communication system;

FIG. 7 shows signal power vs. distance for the system of FIG. 6; and

FIGs. 8 and 9 show the transmitted and received power spectrum for the system of FIG. 6.

Detailed Description

[0014] FIG. 1 schematically depicts a multi-span optical fiber communication system 10, wherein reference numerals 11-13 designate the transmitter, receiver, and optical fiber transmission path that connects transmitter and receiver. The system will typically be a multi-wavelength system having closely spaced (e.g., 1 nm spacing) signal channels. Thus, transmitter 11 actually comprises a multiplicity of transmitters with associated known components, e.g., isolators, polarization controllers, modulators and multiplexers. It typically will also comprise a power amplifier, e.g., an EDFA. Analogously, receiver 12 will typically comprise a multiplicity of receivers, with demultiplexing means for separating the signal channels.

[0015] The optical fiber transmission path comprises one or more repeater spans, indicated by broken vertical lines. In multi-span paths the spans will generally be substantially identical. An exemplary span 20 is schematically shown in FIG. 2, wherein reference numerals 21-22 refer, respectively, to the pump laser, and to a conventional directional coupler (frequently referred to as "WDM") that serves to couple the pump radiation into the transmission path, optionally such that the pump radiation propagates in opposite direction to the signal radiation. Numerals 23-25 refer, respectively, to the transmission fiber, Er-doped fiber, and an optional optical isolator. The "X" symbols indicate fiber splices, as is conventional.

[0016] The pump laser is a high power laser, exemplarily comprising a dual-clad fiber pumped by an array of 915 nm laser diodes, with the output of the dual-clad fiber converted to the desired wavelength through cascaded Raman lasers. See, for instance, the above cited paper by S. G. Grubb et al. Pump lasers of this type are commercially available and are capable of providing more than 1W of optical power at a desired wavelength in the approximate range 1450-1500 nm.

[0017] The transmission fiber 23 in FIG. 2 can be conventional Ge-doped silica-based fiber, exemplarily commercially available dispersion-shifted fiber with dispersion zero at about 1580 nm. By way of example, the length of the transmission fiber is of order 100 km.

[0018] When pumped by means of the pump laser in known manner, Er-doped fiber 24 acts as optical amplifier for signal radiation of approximate wavelength 1.55 μm . The direction of signal propagation is indicated by arrows in FIG. 2. As is known, in the presence of pump radiation of appropriate wavelength, signal radiation in the transmission fiber can experience gain due to stimulated Raman scattering (SRS). Thus, span 20 contains two gain elements, namely, EDFA 24 and a distributed Raman amplifier in the transmission fiber 23. For the exemplary

configuration shown in FIG. 2, EDFA 24 is a remotely pumped amplifier.

[0019] FIG. 3 shows the Raman gain spectrum of a typical Ge-doped silica fiber. As can be seen, the gain has a pronounced maximum for a wavelength difference between signal and pump that corresponds to a frequently shift of about 13 THz. For signal radiation of 1550 nm, pump radiation of about 1450 nm wavelength provides maximum Raman gain.

[0020] By definition, a remotely pumped optical fiber communication system comprises a conventional erbium-doped fiber amplifier and a distributed Raman amplifier disposed between the pump source and said fiber amplifier, with conventional silica-based transmission fiber providing the Raman gain medium.

[0021] As stated above, conventional EDFAs typically perform optimally if pumped with 1480 nm radiation.

[0022] We have discovered that significant performance improvements can be obtained if the wavelength in a remotely pumped system is selected to be greater than the wavelengths which result in optimal performance for the EDFA or for a Raman amplifier. More specifically, by selecting the pump radiation source such that $\lambda_p \geq 1490$ nm, it is possible to reduce deleterious MPI and thereby obtain improved overall performance. This is especially the case for multi-stage remotely pumped optical fiber communication systems such as undersea systems of length ≥ 1000 km.

[0023] By way of example, for a signal of wavelength 1558 nm, maximum Raman gain in a given conventional Ge-doped silica-based transmission fiber is obtained with a pump wavelength of about 1458 nm. Conventional Er-doped amplifier fiber has optimal performance if pumped at 1480 nm. Thus, pump radiation of wavelength 1490 nm differs substantially from the optimal pump wavelengths for either an EDFA or a Raman amplifier, respectively. However, use of 1490 nm pump radiation can result in improved performance of a remotely pumped optical fiber communication system due, at least in part, to reduced MPI.

[0024] FIG. 4 illustrates the above discussion. The data of FIG. 4 pertains to the combined Raman and erbium-doped amplifiers in an exemplary remotely pumped optical fiber communication system with 22 identical stages, the stages being similar to those described below. The figure shows signal to noise ratio as a function of pump wavelength (pump power 1.1 watt), for two contributing noise mechanisms, namely, amplified spontaneous emission or ASE (curve 41) and MPI (curve 42). As can be seen from the figure, the noise due to ASE is relatively independent of pump wavelength, but the signal to noise ratio due to MPI increases strongly with increasing pump wavelength, at least up to about 1490 nm. FIG. 4 thus clearly demonstrates a benefit that results from detuning of the pump wavelength, as described above. At higher pump powers even longer pump wavelengths can yield improved performance.

[0025] FIG. 5 shows gain (curve 51) and noise figure (curve 52) as a function of pump wavelength for an exemplary EDFA (length 22 meters, pump power 10mW, signal power -6 dBm). As can be seen, the gain and noise figure vary relatively slowly as a function of pump wavelength, facilitating design of "detuned" remotely pumped optical fiber communication systems according to the invention.

[0026] FIG. 6 schematically depicts one stage 60 in a further exemplary remotely pumped system. The system was implemented in a test bed, simulating transmission over 5280 km with 8 channels, each at 2.5 Gbit/s. Each repeater span was 240 km long. The system achieved a performance comparable to that of a similar system using conventional locally pumped EDFAs with 80 km repeater span, thereby demonstrating the saving in repeater cost and improvement in reliability that are attainable with remotely pumped systems.

[0027] In FIG. 6, numerals 61 and 62 refer to a first and an adjacent second repeater, respectively. Numerals 631-636 each refer to 80 km of transmission fiber, the transmission fiber being commercially available dispersion shifted fiber, with appropriate lengths of dispersion compensating fiber added. This is not shown in the figure. Numerals 641 and 642 each refer to 80 km of low loss, pure silica-core transmission fiber, used to provide pump power to remotely located EDFAs 652 and 655. Numerals 651-655 refer to Er-doped fiber, numerals 661-664 refer to WDMs, and numerals 671-674 refer to pump lasers. FIG. 6 also shows several optical isolators, but does not show splices.

[0028] Pump radiation (1485 nm) from pump source 672 remotely pumps EDFA 652 through 80 km of low loss, pure silica-core fiber 641 and WDM 662. Pump radiation (1495 nm) from pump 673 (corresponding to pump 671 in repeater 61) is provided to EDFAs 654 and 653, with 80 km of transmission fiber 634 between the EDFAs. The transmission fiber provides Raman gain to the signal radiation that propagates in the direction from repeater 61 to repeater 62.

[0029] The transmission fiber consisted of dispersion-shifted fiber with zero dispersion wavelength at about 1580 nm and about -2 ps/nm · km chromatic dispersion at the signal wavelength. Accumulated dispersion was compensated every 480 km with conventional single mode fiber with chromatic dispersion of about 17 ps/nm · km. Additional dispersion compensation was provided at the receiver (not shown). Gain equalization was provided every 480 km (not shown). Three conventional isolators in each span served to reduce MPI caused by double Rayleigh reflections.

[0030] The pump lasers were formed by pumping a dual clad fiber with 915 nm radiation from a laser diode array such that pump radiation of a desired wavelength was formed in known manner. Each pump source was capable of launching about 1.2 W of optical power into a single mode fiber.

[0031] FIG. 7 shows the signal power evolution during transmission through one span, starting at EDFA 651 and ending with the Raman amplification in transmission fiber 635.

[0032] FIG. 8 shows the transmitted power spectrum, and FIG. 9 shows the received spectrum, after 5280 km transmission. At the receiver, the signal to noise ratio was approximately 11 dB.

[0033] The above described remotely pumped exemplary optical fiber system comprises features that serve to reduce MPI. However, MPI was still present to some degree. It can be further reduced in a communication system according to the invention, with the pump radiation further detuned from the wavelength of maximum Raman gain, as described above.

Claims

1. An optical fiber communication system (10) comprising a transmitter (11) for transmitting a signal, a receiver (12), an optical fiber transmission link (13) that signal-transmissively connects the transmitter and the receiver and comprises at least one erbium-doped optical fiber amplifier (24), and a source of pump radiation of wavelength λ_p less than the wavelength λ_s of the signal, said source (21) of pump radiation being spaced from said erbium-doped optical fiber amplifier, with the pump radiation being transmitted to the erbium-doped optical fiber amplifier through at least a portion of said optical fiber transmission link that comprises silica-based single mode optical fiber selected to provide Raman gain at the signal wavelength;
 wherein λ_p is selected to be longer than an optimal wavelength $\lambda_{p,Raman}$ for producing said Raman gain, and also to be longer than an optimal wavelength $\lambda_{p,EDFA}$ for pumping the Er-doped optical fiber amplifier, CHARACTERIZED IN THAT λ_p is in the range of 1490-1510nm, but excluding the wavelengths 1490 and 1495nm, with λ_s being approximately equal to 1.55 μ m, whereby low multi-path interference results.
2. System according to claim 1, wherein said optical fiber transmission link comprises a multiplicity of substantially identical repeater spans.
3. System according to claim 2, wherein a given one of said repeater spans is more than 100 km long.
4. System according to claim 3, wherein the source of pump radiation of the given repeater span is a diode-pumped fiber laser.
5. A method for providing optical pump power to an optical fiber communication system (10) having a transmission path that includes at least one rare-earth doped optical fiber amplifier (24), operating at a first pump wavelength, that by itself provides a system response at a given optimization level, said method comprising the steps of:
 remotely pumping said communication system through at least a portion of said transmission path to generate Raman gain in said transmission path portion and stimulated gain in said rare-earth doped optical fiber amplifier at a second pump wavelength;
 wherein said second pump wavelength is selected to be greater than said first pump wavelength and greater than a third pump wavelength generating a substantially maximum amount of Raman gain in said transmission path portion, wherein said second pump wavelength is less than a signal wavelength;
 CHARACTERIZED IN THAT said second pump wavelength is in the range 1490-1510nm, but excluding the wavelengths 1490 and 1495nm, the signal wavelength being approximately equal to 1.55 μ m.
6. A method for providing optical pump power to an optical fiber communication system (10) having a rare-earth doped optical fiber amplifier (24) and a Raman amplifier such that a given level of multipath interference (MPI) is produced when said amplifiers are pumped at a first wavelength that is less than a signal wavelength;
 wherein said method comprises the steps of:
 selecting a pump wavelength greater than said first wavelength;
 remotely pumping said rare-earth doped optical fiber amplifier and said Raman amplifier at said pump wavelength, CHARACTERIZED IN THAT said pump wavelength is in the range 1490-1510nm, but excluding the wavelengths 1490 and 1495nm, and said signal wavelength is approximately equal to 1.55 μ m, whereby MPI is produced at a level below said given level of MPI.

Patentansprüche

- 5 1. Faseroptisches Kommunikationssystem (10) mit einem Sender (11) zum Senden eines Signals, einem Empfänger (12), einer faseroptischen Übertragungsstrecke (13), die den Sender und den Empfänger signalübertragend verbindet und mindestens einen erbiumdotierten optischen Faserverstärker (24) umfaßt, und einer Quelle von Pumpstrahlung einer Wellenlänge λ_p , die kleiner als die Wellenlänge λ_s des Signals ist, wobei die Quelle (21) von Pumpstrahlung von dem erbiumdotierten optischen Faserverstärker beabstandet ist, wobei die Pumpstrahlung durch

10 mindestens einen Teil der faseroptischen Übertragungsstrecke, der Einmoden-Lichtleitfaser auf Silika-Basis umfaßt, die so gewählt wird, daß sie bei der Signalwellenlänge eine Raman-Verstärkung bereitstellt, zu dem erbiumdotierten optischen Faserverstärker gesendet wird;

wobei λ_p größer als eine optimale Wellenlänge $\lambda_{p,Raman}$ für die Erzeugung der Raman-Verstärkung und außerdem größer als eine optimale Wellenlänge $\lambda_{p,EDFA}$ für das Pumpen des Er-dotierten optischen Faserverstärkers

15 gewählt wird,

dadurch gekennzeichnet, daß

λ_p im Bereich von 1490-1510 nm, aber nicht bei den Wellenlängen 1490 und 1495 nm liegt, wobei λ_s ungefähr gleich 1,55 μm ist, wodurch sich eine geringe Mehrwegestörung ergibt.
- 20 2. System nach Anspruch 1, wobei die faseroptische Übertragungsstrecke eine Vielzahl im wesentlichen identischer Zwischenverstärkerspannen umfaßt.
3. System nach Anspruch 2, wobei eine gegebene der Zwischenverstärkerspannen mehr als 100 km lang ist.
- 25 4. System nach Anspruch 3, wobei die Quelle von Pumpstrahlung der gegebenen Zwischenverstärkerspanne ein diodengepumpter Faserlaser ist.
5. Verfahren zur Bereitstellung von optischer Pumpleistung für ein faseroptisches Kommunikationssystem (10) mit einem Übertragungsweg, der mindestens einen seltenerddotierten optischen Faserverstärker (24) enthält, der mit

30 einer ersten Pumpwellenlänge arbeitet, wodurch für sich ein Systemansprechverhalten auf einem gegebenen Optimierungsniveau bereitgestellt wird, mit den folgenden Schritten:

Fernpumpen des Kommunikationssystems durch mindestens einen Teil des Übertragungswegs, um in dem Übertragungswegteil eine Raman-Verstärkung und bei einer zweiten Pumpwellenlänge eine stimulierte

35 Verstärkung in dem seltenerddotierten optischen Faserverstärker zu erzeugen;

wobei die zweite Pumpwellenlänge größer als die erste Pumpwellenlänge und größer als eine dritte Pumpwellenlänge gewählt wird, die einen im wesentlichen maximalen Betrag Raman-Verstärkung in dem Übertragungswegteil erzeugt, wobei die zweite Pumpwellenlänge kleiner als eine Signalwellenlänge ist;

40 dadurch gekennzeichnet, daß

die zweite Pumpwellenlänge im Bereich von 1490-1510 nm, aber nicht bei den Wellenlängen 1490 und 1495 nm liegt, wobei die Signalwellenlänge ungefähr gleich 1,55 μm ist.
- 45 6. Verfahren zur Bereitstellung von optischer Pumpleistung für ein faseroptisches Kommunikationssystem (10) mit einem seltenerddotierten optischen Faserverstärker (24) und einem Raman-Verstärker, so daß ein gegebener Pegel der Mehrwegestörung (MPI) erzeugt wird, wenn die Verstärker mit einer ersten Wellenlänge gepumpt werden, die kleiner als eine Signalwellenlänge ist;

50 wobei das Verfahren die folgenden Schritte umfaßt:

Wählen einer Pumpwellenlänge, die größer als die erste Wellenlänge ist;

Fernpumpen des seltenerddotierten optischen Faserverstärkers und des Raman-Verstärkers mit der

55 Pumpwellenlänge,

dadurch gekennzeichnet, daß
 die Pumpwellenlänge im Bereich von 1490-1510 nm, aber nicht bei den Wellenlängen 1490 und 1495 nm liegt
 und die Signalwellenlänge ungefähr gleich 1,55 μm ist, wodurch MPI mit einem Pegel erzeugt wird, der unter dem
 gegebenen Pegel der MPI liegt.

5

Revendications

10

1. Système de communication à fibre optique (10) comprenant un émetteur (11) pour émettre un signal, un récepteur (12), une liaison de transmission par fibre optique (13) qui connecte par transmission de signal l'émetteur et le récepteur et comprend au moins un amplificateur à fibre optique dopée à l'erbium (24), et une source de rayonnement de pompage d'une longueur d'onde λ_p inférieure à la longueur d'onde λ_s du signal, ladite source (21) de rayonnement de pompage étant espacée dudit amplificateur à fibre optique dopée à l'erbium, le rayonnement de pompage étant transmis jusqu'à l'amplificateur à fibre optique dopée à l'erbium à travers au moins une partie de ladite liaison de transmission par fibre optique qui comprend une fibre optique monomode à base de silice sélectionnée en vue de fournir un gain Raman à la longueur d'onde du signal ;

15

dans lequel λ_p est sélectionnée afin d'être plus longue qu'une longueur d'onde optimale $\lambda_{p,\text{Raman}}$ pour produire ledit gain Raman, et aussi afin d'être plus longue qu'une longueur d'onde optimale $\lambda_{p,\text{EDFA}}$ pour pomper l'amplificateur à fibre optique dopée à l'erbium,

20

CARACTERISE EN CE QUE

λ_p se situe dans la gamme de 1490 à 1510 nm, mais excluant les longueurs d'onde de 1490 et 1495 nm, λ_s étant approximativement égale à 1,55 μm , donnant ainsi lieu à un brouillage dû à la propagation par trajet multiple faible.

25

2. Système selon la revendication 1, dans lequel ladite liaison de transmission par fibre optique comprend une multiplicité de longueurs de répétition sensiblement identiques.

3. Système selon la revendication 2, dans lequel une longueur donnée desdites longueurs de répétition est de plus de 100 km de long.

30

4. Système selon la revendication 3, dans lequel la source de rayonnement de pompage de la longueur de répétition donnée est un laser à fibre pompée par diode.

35

5. Procédé pour fournir une puissance de pompage optique à un système de communication à fibre optique (10) ayant un trajet de transmission qui comporte au moins un amplificateur à fibre optique dopée aux terres rares (24), fonctionnant à une première longueur d'onde de pompage, qui fournit à lui seul une réponse de système à un niveau d'optimisation donné, ledit procédé comprenant les étapes de :

40

pompage à distance dudit système de communication à travers au moins une partie dudit trajet de transmission en vue de générer le gain Raman dans ladite partie de trajet de transmission et le gain stimulé dans ledit amplificateur à fibre optique dopée aux terres rares à une deuxième longueur d'onde de pompage ;

45

dans lequel ladite deuxième longueur d'onde de pompage est sélectionnée afin d'être supérieure à ladite première longueur d'onde de pompage et supérieure à une troisième longueur d'onde de pompage générant une quantité substantiellement maximum de gain Raman dans ladite partie de trajet de transmission, dans lequel ladite deuxième longueur d'onde de pompage est inférieure à une longueur d'onde de signal ;

CARACTERISE EN CE QUE

50

ladite deuxième longueur d'onde de pompage se situe dans la gamme de 1490 à 1510 nm, mais excluant les longueurs d'onde de 1490 et 1495 nm, la longueur d'onde de signal étant approximativement égale à 1,55 μm .

55

6. Procédé pour fournir une puissance de pompage optique à un système de communication à fibre optique (10) ayant un amplificateur à fibre optique dopée aux terres rares (24) et un amplificateur Raman de telle sorte qu'un niveau donné de brouillage dû à la propagation par trajet multiple (MPI) soit produit quand lesdits amplificateurs sont pompés à une première longueur d'onde qui est inférieure à une longueur d'onde de signal ;

dans lequel ledit procédé comprend les étapes de :

sélection d'une longueur d'onde de pompage supérieure à ladite première longueur d'onde ;

pompage à distance dudit amplificateur à fibre optique dopée aux terres rares et dudit amplificateur Raman à ladite longueur d'onde de pompage,

5

CARACTERISE EN CE QUE

ladite deuxième longueur d'onde de pompage se situe dans la gamme de 1490 à 1510 nm, mais excluant les longueurs d'onde de 1490 et 1495 nm, et ladite longueur d'onde de signal est approximativement égale à 1,55 μm , si bien qu'un MPI est produit à un niveau inférieur audit niveau donné de MPI.

10

15

20

25

30

35

40

45

50

55

FIG. 1

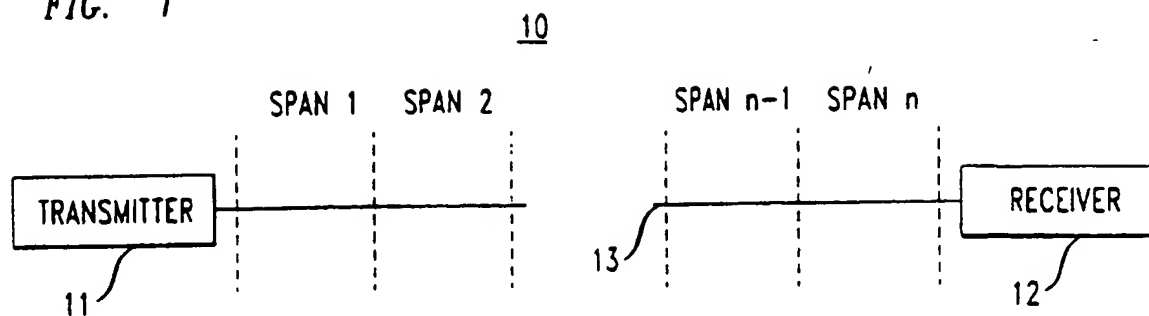


FIG. 2

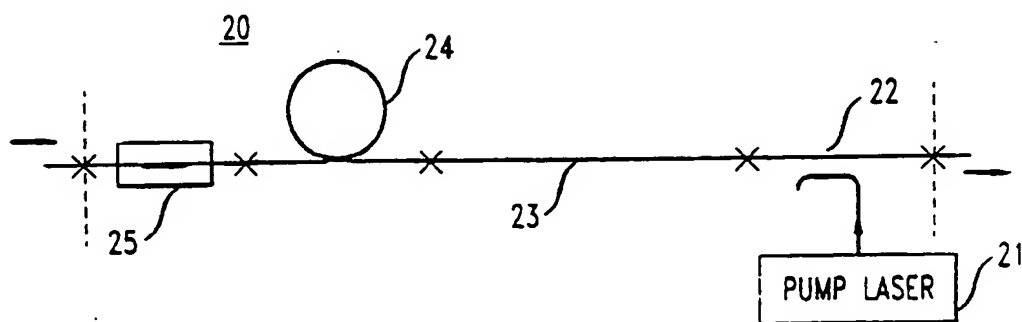


FIG. 3

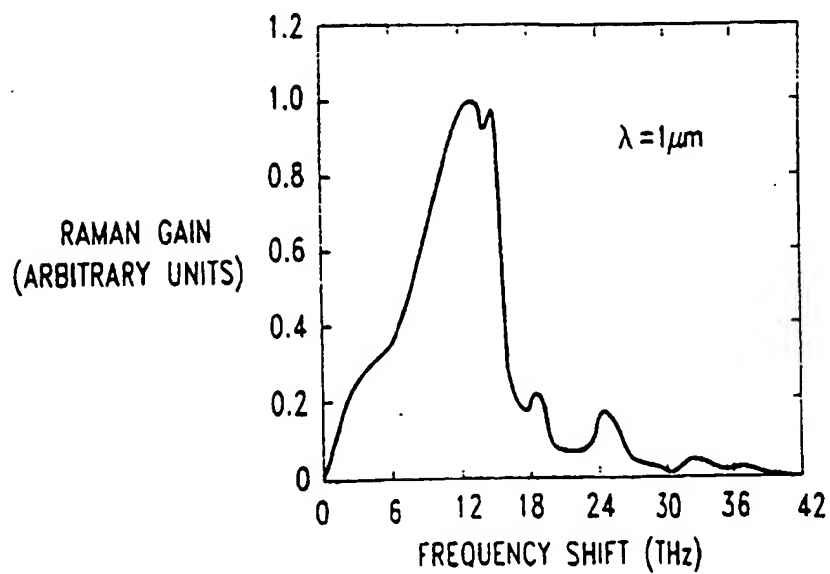


FIG. 4

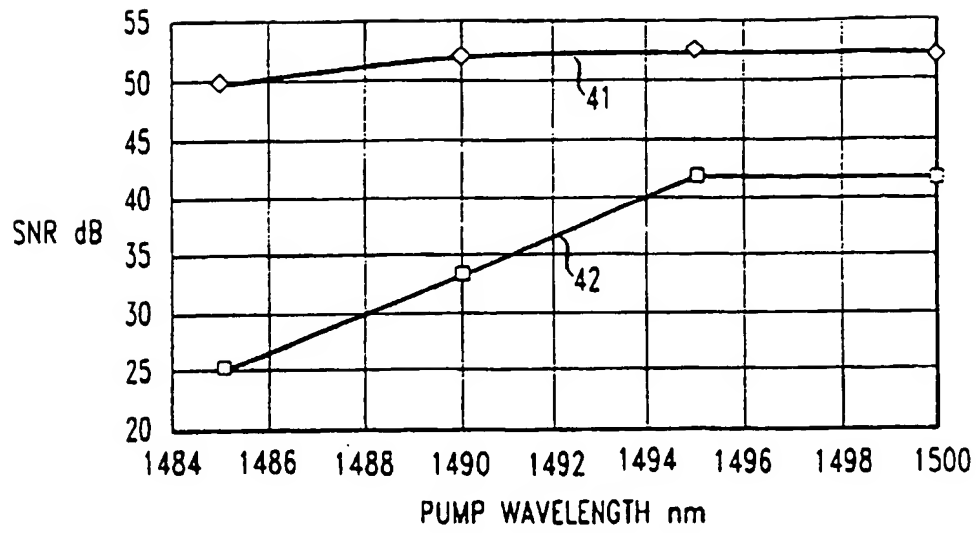


FIG. 5

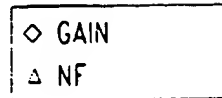
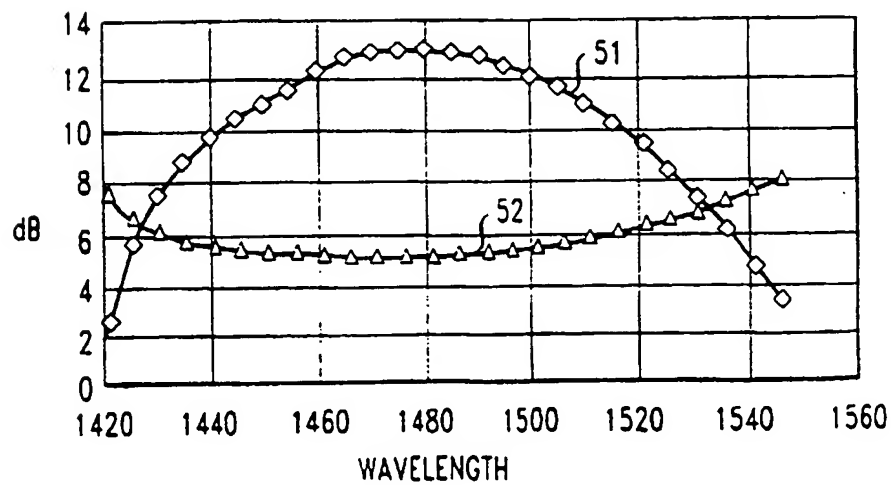


FIG. 6

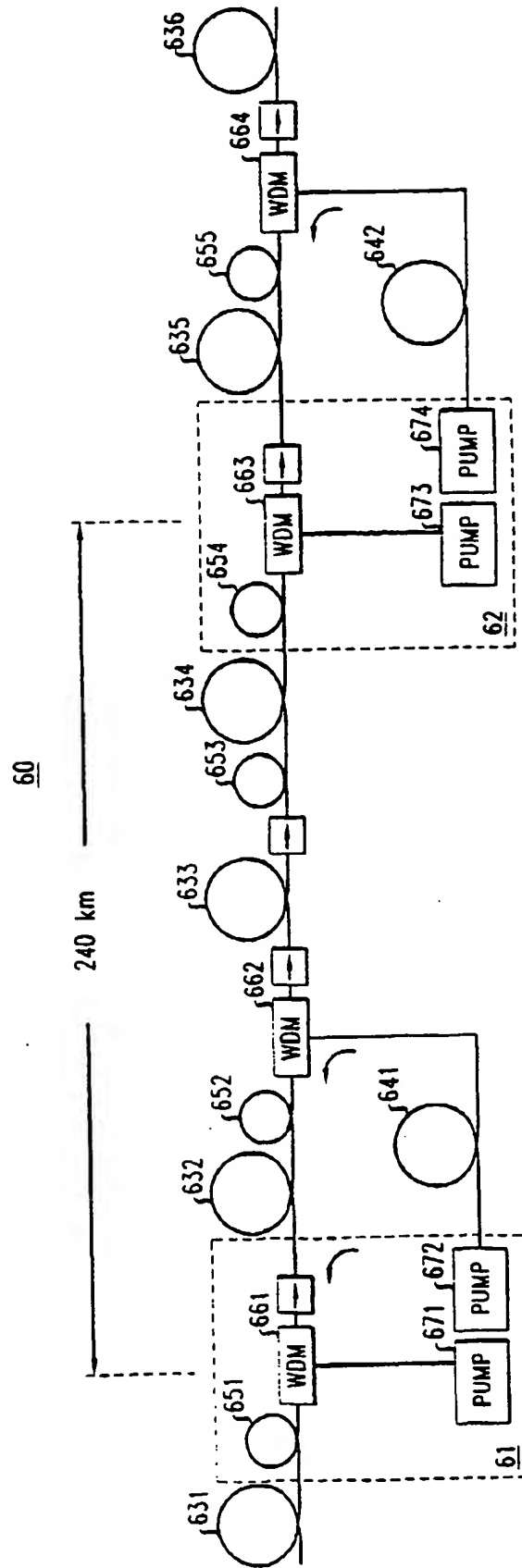


FIG. 7

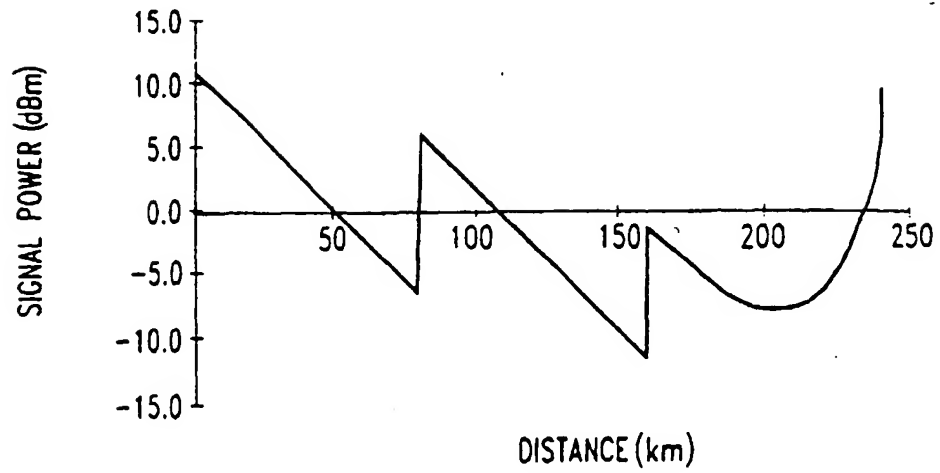


FIG. 8

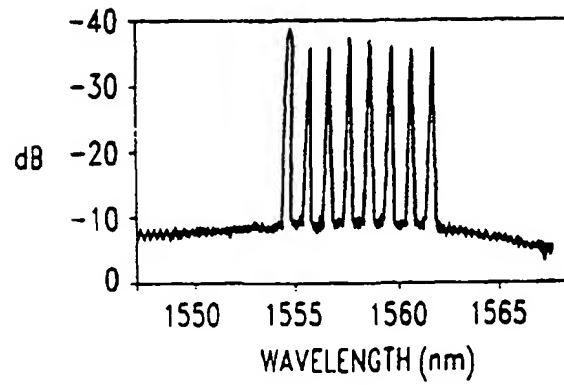


FIG. 9

